

The mathematics behind next generation bone prostheses

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Joint work with Dr Andrew Cramer & A/Prof Tony Roberts
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Femoral bone implants

(A)



(B)



(C)



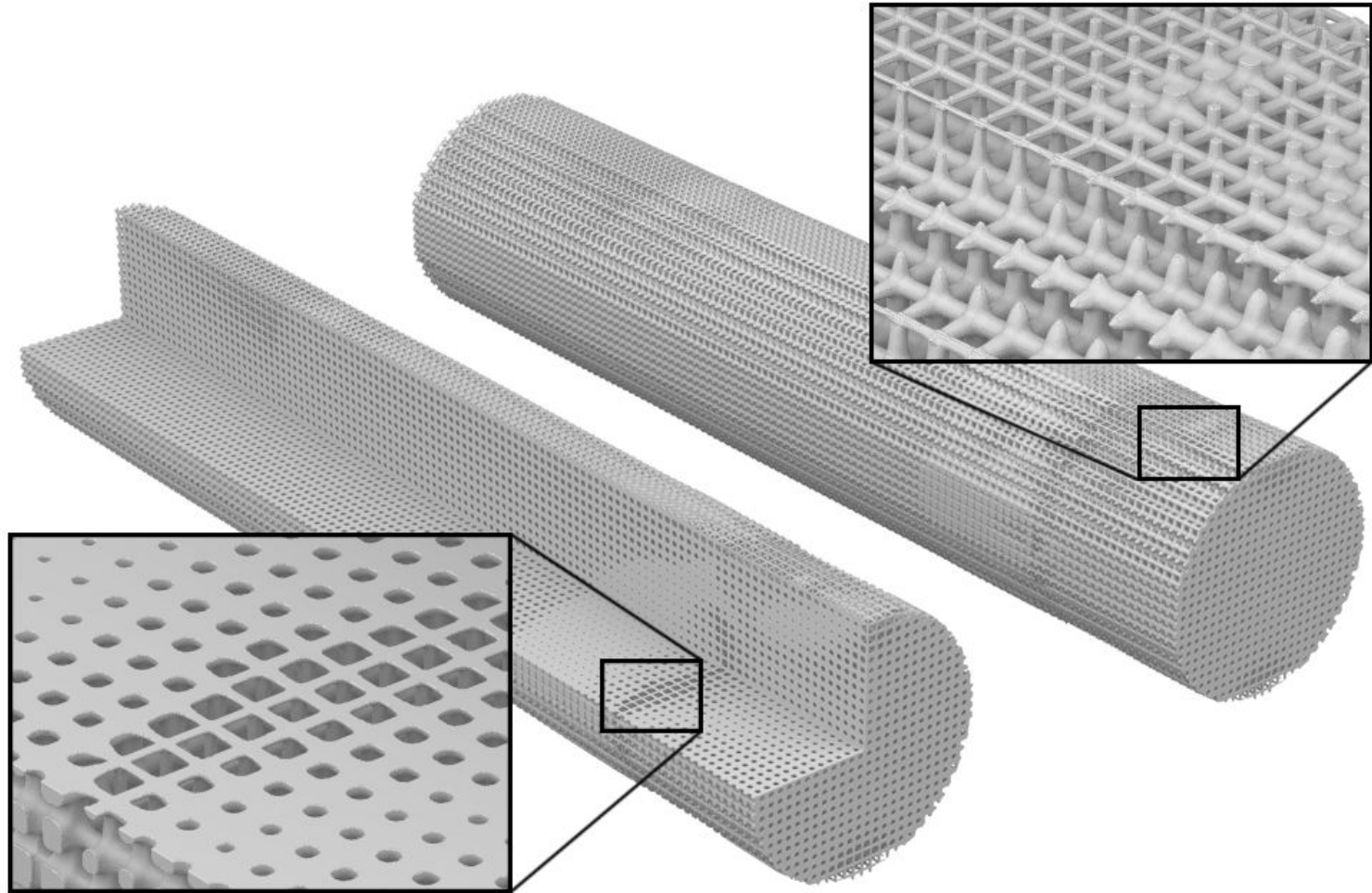
From Benjamin JB, Lund PJ. Orthopedic devices. In: Hunter TB, Bragg DG, eds. Radiologic Guide to Medical Devices and Foreign Bodies, St Louis, MO: Mosby-Year Book, 1994, 348-385.



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Create change

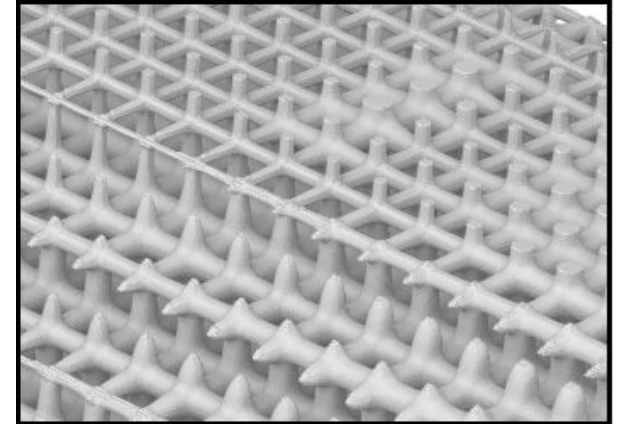
Looking to the future: Porous implants?



A multiscale design problem

Microstructure requirements

- Porous labyrinths for bone in-growth
- Mechanical stiffness & strength
- Manufacturability



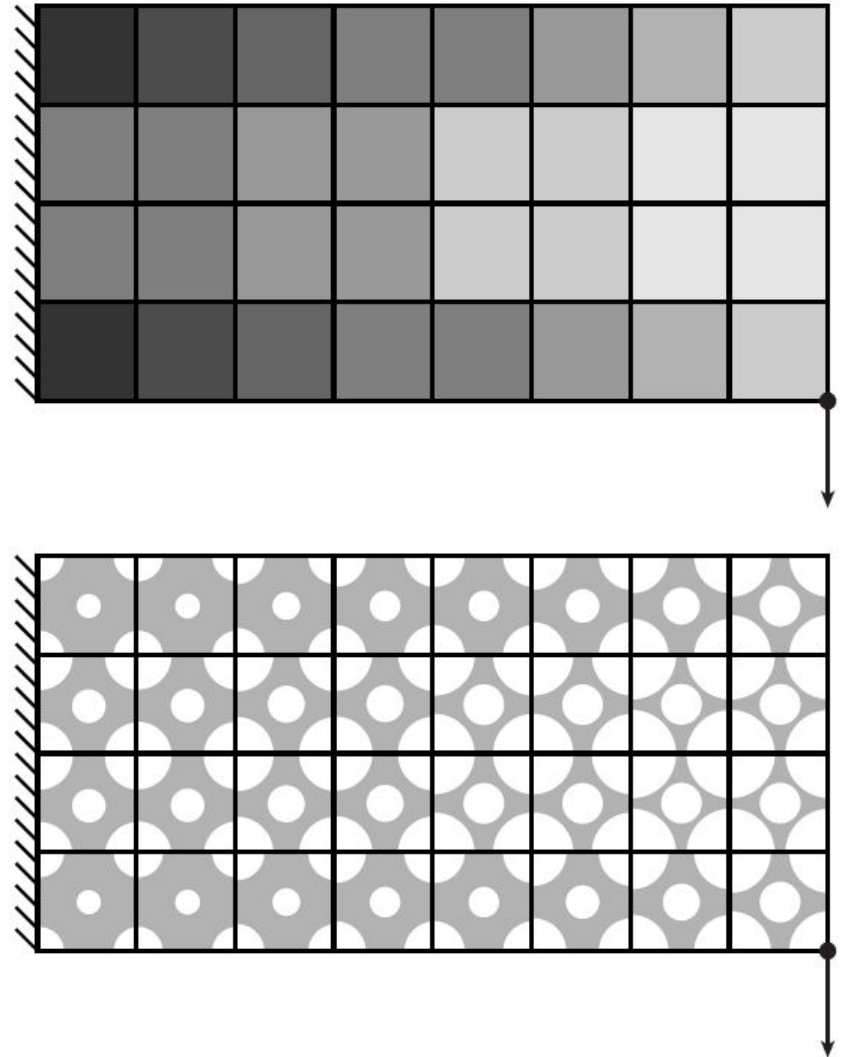
Macroscopic requirements

- Overall shape & size
- Mechanical stiffness and strength, including fatigue
- Minimal bone resorption
- Reduced shear stress along bone/implant interface
- Connectivity of microstructures

Our approach

Design the microstructure family first.

Each element in the macroscopic design uses a microstructure from our set.



Where is the mathematics?

Equations of solid mechanics

- Derivatives
- Integrals
- Simultaneous equations



strain $\epsilon = \frac{du}{dx}$ displacement

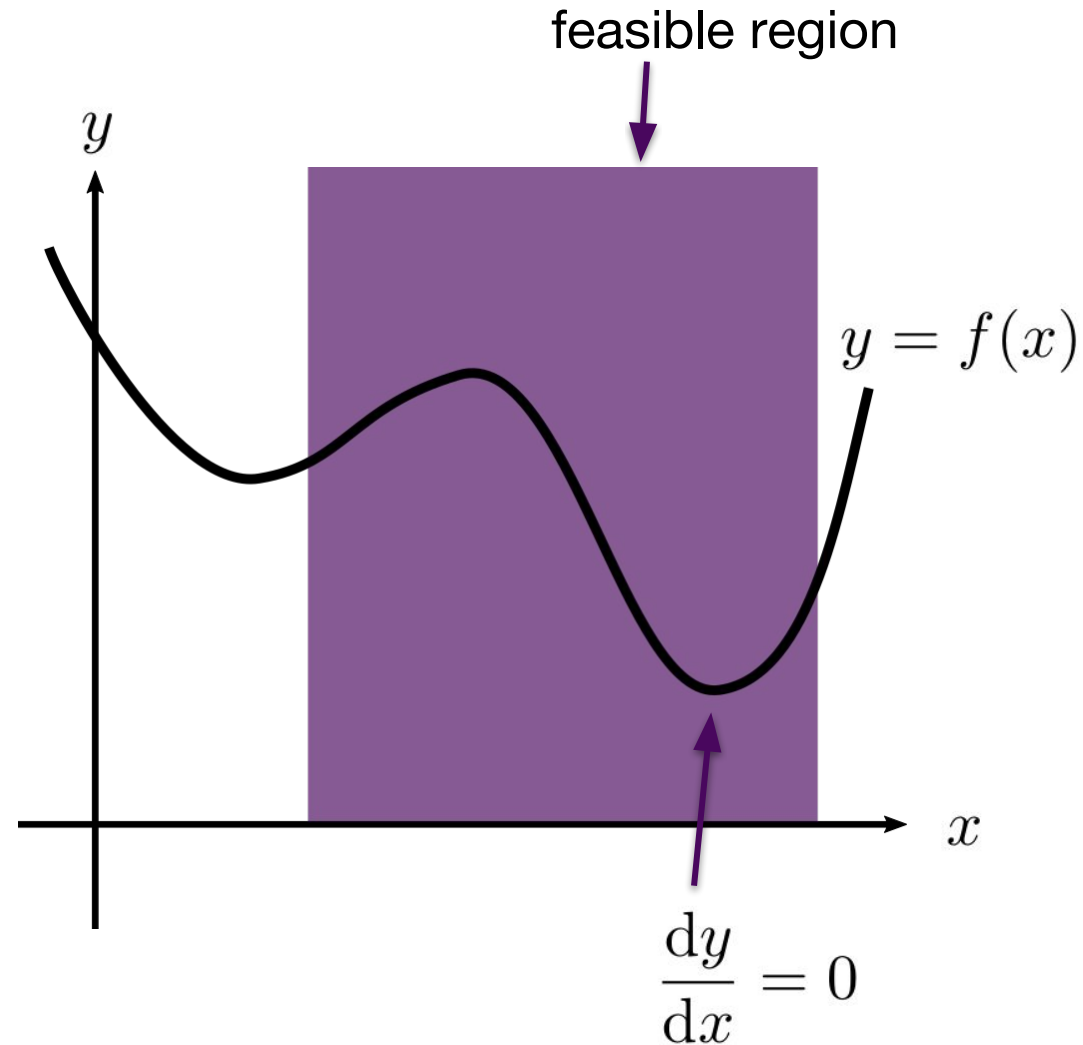
stress $\sigma = E\epsilon$ Young's modulus

$\frac{d\sigma}{dx} + b = 0$ body forces spatial coordinate

Where is the mathematics?

Optimisation

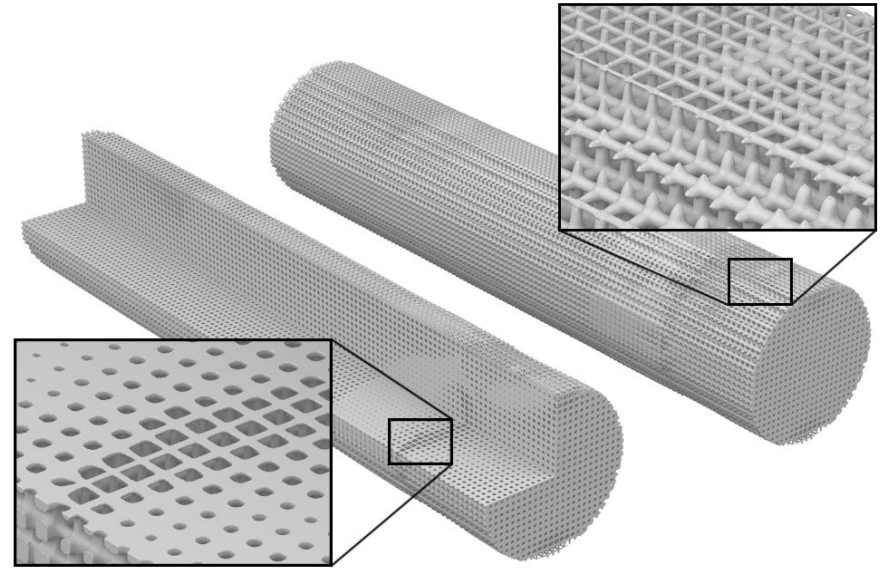
- Derivatives
- Minimisation
- Feasible region



A sense of scale

Microstructure design

- Matrix equations $\approx 780,000$ unknowns
- Minimisation $\approx 260,000$ variables

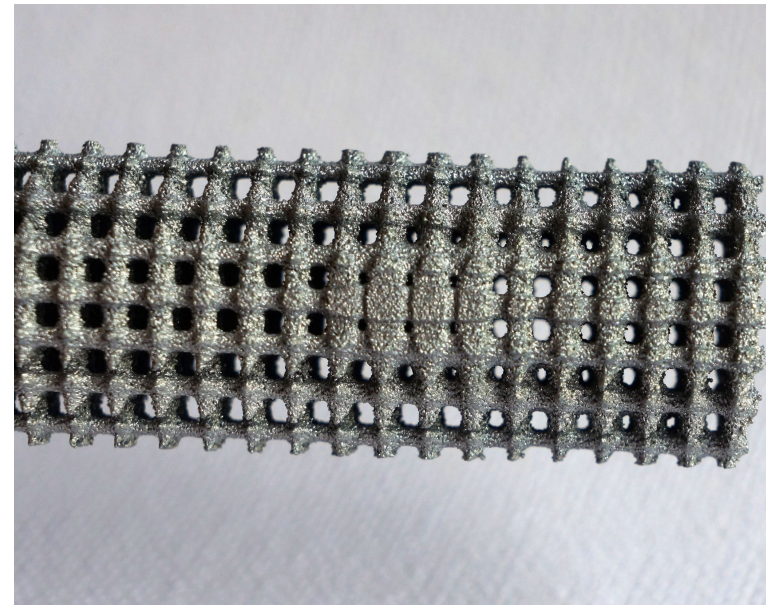
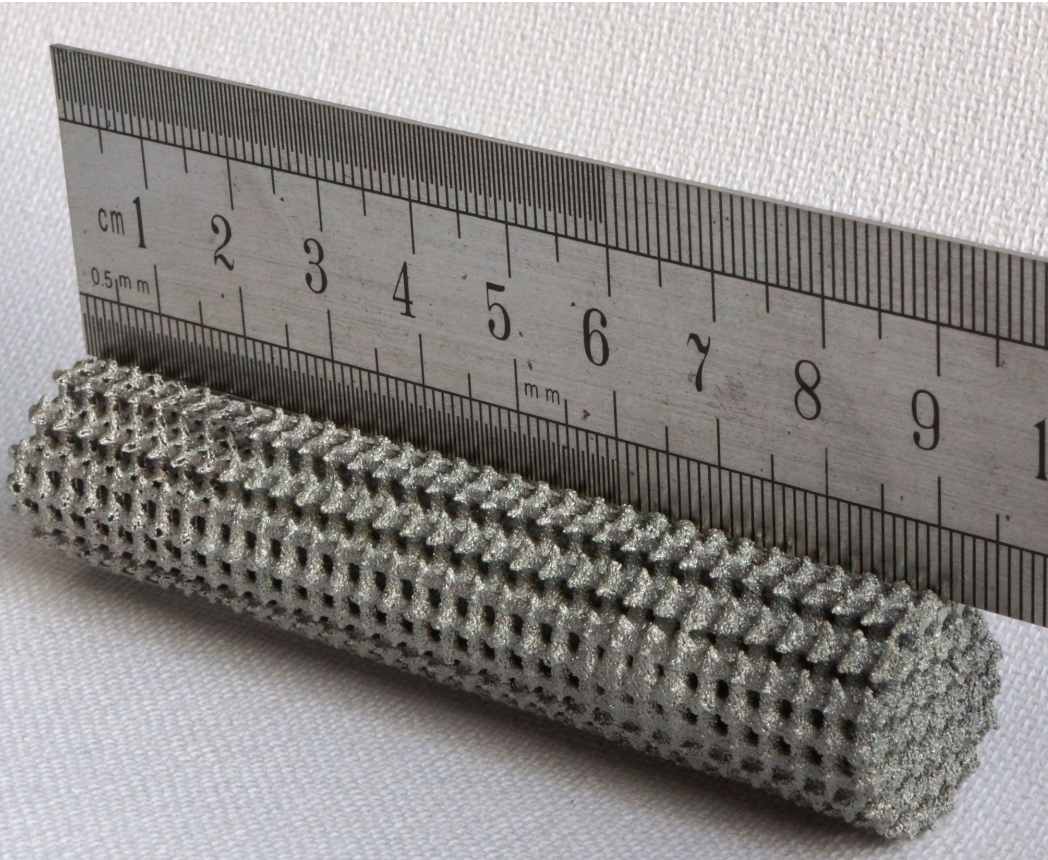
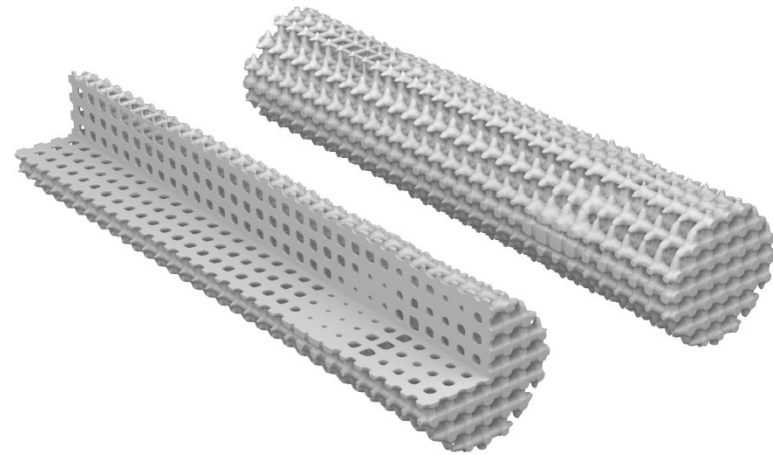


Macroscopic optimisation

- Matrix equations ≈ 16 million unknowns
- Minimisation ≈ 2 million variables



3D-printed prototype



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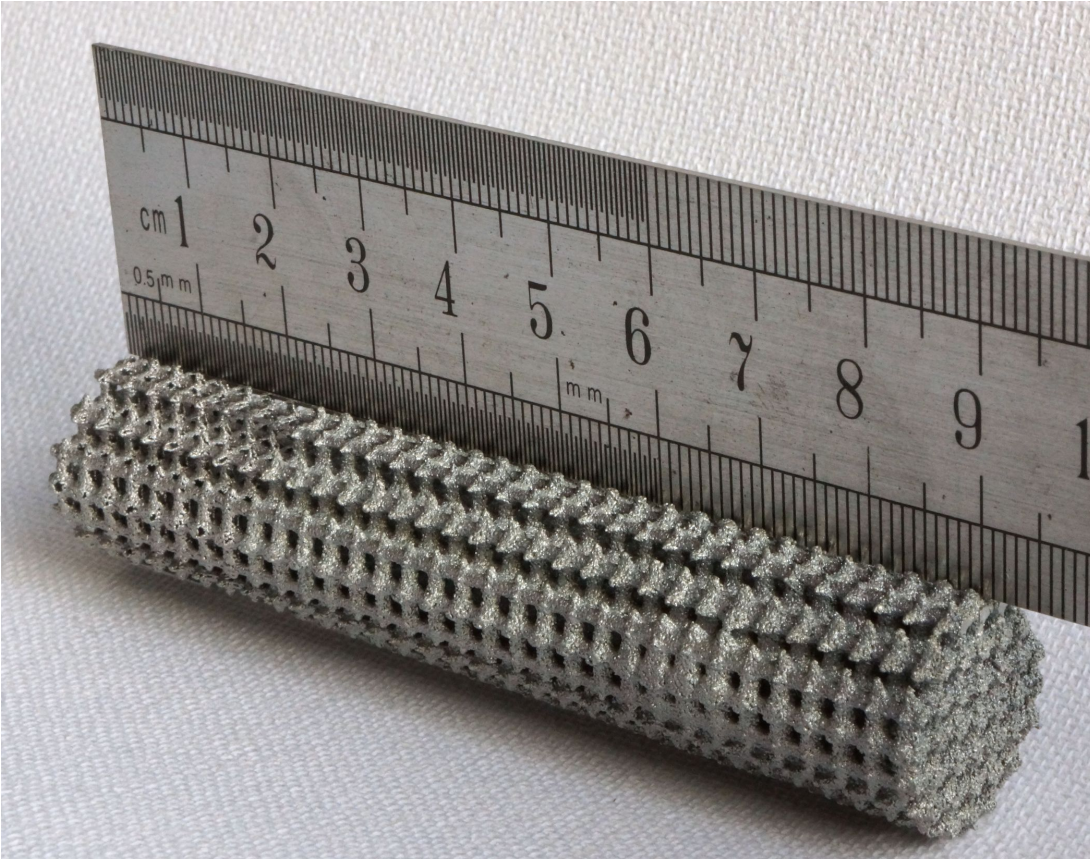
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Macroscopic design

- Minimise shear stress on Π
- Subject to constrained bone resorption (5 %)

$$F = \int_{\Pi} (\tau_i \tau_i)^m dS = \int_{\Pi} \tau^{2m} dS$$

$$m_r = \frac{1}{|\Omega_B|} \int_{\Omega_B} H((1-s)U_{\text{ref}} - U) \rho d\mathbf{x}$$

